



Facile and green synthetic strategy of birnessite-type MnO_2 with high efficiency for airborne benzene removal at low temperatures

Yang Liu^{a,*}, Hao Zhou^a, Ranran Cao^b, Xingyun Liu^a, Pengyi Zhang^{b,*}, Jingjing Zhan^a, Lifan Liu^a

^a Key Laboratory of Industrial Ecology and Environmental Engineering (Ministry of Education), School of Food and Environment, Dalian University of Technology, Panjin, 124221, China

^b School of Environment, Tsinghua University, Beijing, 100084, China

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ABSTRACT

Volatile organic compounds (VOCs) are notorious for global air pollution. It is key to find a material with high and stable activity to catalytically oxidize VOCs at low temperatures. In this paper, benzene, as a typical VOC contaminant, could be completely oxidized on a highly efficient and moisture-resistant birnessite MnO_2 at temperatures significantly lower than the reported values in literature. The best catalyst (H-MnO_2 (30-0.2-6)) could be tailored via a facile and green process by engineering a proper combination of treatment temperature (30 °C), HNO_3 aqueous concentration (0.2 M) and treatment period (6 h). The thus-obtained MnO_2 exhibited a stable removal efficiency of ~94% for 318 ppm of benzene under a high space velocity of $120 \text{ L} \cdot \text{g}^{-1} \cdot \text{h}^{-1}$ and 1.5 vol.% H_2O at 250 °C. XRD, SEM, (HR)TEM, EDS mapping, XPS, H_2 -TPR, O_2 -TPD and pyridine adsorption IR were combined with the deliberately designed C_6H_6 -TPD, surface oxidation reaction of benzene and CO_2 -TPD to disclose the tremendous role of acid treatment in benzene oxidation. The increased acid sites and acidity of the acid-treated surface promoted the adsorption and activation of gaseous benzene, and the lattice oxygen and surface adsorbed oxygen became more facile and reactive due to the generated active oxygen vacancies via acid treatment, these two favorable factors together with the easy desorption of reaction products resulting in the excellent performance of the acid-treated sample. Finally, the acid treatment method can be extended to most of other crystal structures of manganese dioxides except α - MnO_2 .

1. Introduction

According to the annual report of the *State of Global Air 2018* [1], air pollution is the leading environmental cause of death worldwide and is the 4th highest cause of death among all health risks, especially in the developing countries. For example, China and India now are among the highest air pollution health burdens in the world. Volatile organic compounds (VOCs) are notorious for the global air pollution. They are also the precursors of ozone, photochemical smog and secondary aerosols [2]. As one of the most abundant VOCs in polluted air, benzene is extremely difficult to decompose and can transport in a long distance, which is posing a great threat to human health and environmental development. As released by the World Health Organization [3], human exposure to benzene has been associated with a range of acute and long-term adverse health effects and diseases, including cancer and aplastic anaemia, etc. Exposure can occur as a result of the ubiquitous use of benzene-containing petroleum products, including motor fuels and solvents; besides, people spending more time indoors are likely to have

higher exposure to benzene due to decorative materials [3].

Hitherto, catalytic oxidation at elevated temperatures has been generally considered as an efficient method to eliminate benzene pollution [4]. And the development of high-performance catalysts is the key issue. For industrial discharging, the catalyst can be coated on to various substrates, such as ceramic honeycomb, cordierite monolith and metal mesh, etc., and the thermal decomposition of residual benzene can be achieved by utilizing the waste heat of the industrial processes; for residential indoor air, although ventilation is a good choice, haze weather that erupts in recent years does not allow people to do so, therefore, it is a good alternative to apply the catalyst to the filter element of an air purifier. The development of noble metals [5–10] and transition metal oxides [11–16] for benzene oxidation has been widely reported in literature. However, the practical application of noble metals is severely hindered by their prohibitively high cost. Benzene oxidation reactions over non-precious metal oxides are mainly focused on the oxides of Cu [11,15], Co [11], Ti [12], V [11,12], Mo [11,13], W [13], Ce [16] and Mn [11,14], etc. Usually catalyst deactivation [17]

* Corresponding authors.

E-mail addresses: liuyang20180129@dlut.edu.cn (Y. Liu), zpy@tsinghua.edu.cn (P. Zhang).

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due to the coexistence of water vapor and other pollutants, e.g., nitrogen compounds, organohalogens and sulfur compounds, etc., is one of the main obstacles restricting their practical uses.

Manganese oxide minerals are ubiquitous in nature, and they are commonly found in terrestrial deposits and ocean nodules [18]. Typically, manganese oxide minerals can be divided into two categories according to the arrangement of the $[\text{MnO}_6]$ octahedra, i.e., the tunnel structure (such as β - MnO_2 , γ - MnO_2 , α - MnO_2 and todorokite MnO_2 , etc., with 1×1 , 1×2 , 2×2 and 3×3 tunnel, respectively) and layer structure (birnessite MnO_2 or δ - MnO_2). Birnessite MnO_2 , which is consisted of sheets of edge-sharing $[\text{MnO}_6]$ octahedra with an interlayer space of $\sim 7 \text{ \AA}$ [19], has been paid much attention in the field of catalysis [20–24]. However, when it comes to benzene oxidation, there are only a few reports using birnessite MnO_2 as catalysts. Li et al. [25] hydrothermally prepared three birnessite MnO_2 with different morphologies, and found that the birnessite nanoflowers, which possessed the highest concentration of oxygen vacancies, were the most active for benzene oxidation. Ye and Dai et al. [26] also investigated the effect of morphology of birnessite MnO_2 on benzene oxidation, and they concluded that the Mn oxide nature, surface lattice oxygen mobility and reducibility were the key factors influencing the catalytic performance. Chen et al. [27] hydrothermally prepared birnessite MnO_2 and investigated the effect of Ti doping on benzene oxidation. Thanks to the active oxygen induced by Ti doping and the abundant pore structures, the Ti-doped sample possessed higher activity. In our previous study [28], the tremendous catalytic enhancement resulted from the exchange of interlayer K^+ of birnessite MnO_2 by Cu^{2+} was reported to be related to the easier reducibility and the higher lattice oxygen reactivity of the Cu-exchanged sample. Although progress has been made in benzene oxidation by using birnessite MnO_2 , the catalytic activity and stability at low reaction temperatures (100 – 200°C), especially under humid reaction condition, still need improving from the viewpoints of energy saving, lowering operation costs and safety, and the conclusions drawn from birnessite MnO_2 have important implications for the development of other kinds of benzene oxidation materials. Herein, redox reaction between KMnO_4 and methanol at low temperature and atmospheric pressure was adopted to fabricate birnessite MnO_2 , which was further treated by HNO_3 aqueous solution at room temperature to obtain efficient and water resistant benzene oxidation material with long-term stability at relatively low reaction temperatures. Acid treatment did not change the crystal structure of birnessite, and this process was GREEN since the HNO_3 solution could be recycled over times. More importantly, acid treatment method can be extended to most of other crystalline MnO_2 catalysts. Finally, comparative characterizations of the physicochemical properties of the catalysts before and after acid treatment together with the temperature programmed desorption of adsorbed benzene and CO_2 and surface oxidation reaction of benzene were performed to explore the intrinsic mechanism of the enhancement of catalytic benzene oxidation by acid treatment.

2. Experimental

2.1. Catalyst synthesis and characterization

All the reagents were used as received without further treatment. The birnessite-type MnO_2 , which was obtained through the redox reaction between KMnO_4 and CH_3OH solution, was denoted as *pristine MnO₂*. Briefly, an appropriate amount of KMnO_4 solid was fully dissolved in deionized water. Then CH_3OH was added into the KMnO_4 solution under constant stirring by magnetic stirrer and the mixture was kept stirring for 12 h. After filtration and washing with deionized water, the obtained solid was dried at 105°C overnight in an oven.

Subsequently, the pristine MnO_2 powder was soaked in HNO_3 solution in a beaker and constantly stirred in a water bath. The mass ratio of solid to liquid was fixed at 1:20. The effects of HNO_3 aqueous concentration, treatment temperature and treatment period were

investigated. After acid treatment, the suspension was filtered and repeatedly washed with deionized water until the pH of the eluate was ~ 7.0 . The resultant solid was then dried at 105°C overnight in an oven. The obtained powder was grounded, tableted, crushed and sieved to 40–60 mesh. For convenience, the acid-treated MnO_2 was denoted as *H-MnO₂* (*T-C-t*), where *T*, *C* and *t* represent the treatment temperature ($^\circ\text{C}$), HNO_3 aqueous concentration (M) and treatment period (h), respectively.

In order to test the universality of the HNO_3 treatment method for other MnO_2 materials, the pristine β - MnO_2 (1×1 tunnel), α - MnO_2 (2×2 tunnel) and todorokite MnO_2 (3×3 tunnel) were prepared according to reference [29–31], respectively, and a commercial MnO_2 (CAS: 1313-13-9) purchased from the Aladdin company was also used. The acid treatment of these four samples was carried out under the optimal conditions (*T*, *C* and *t*) obtained from the birnessite MnO_2 .

For details of the instruments, procedures and parameters used for the characterizations of the surface and bulk properties of the catalysts, see the electronic supplementary information.

2.2. Gaseous benzene oxidation

Catalytic benzene oxidation was performed in a continuous-flow fixed quartz tube reactor with an inner diameter of 6 mm loaded with $\sim 0.1 \text{ g}$ of catalyst under atmospheric pressure. $200 \text{ mL}\cdot\text{min}^{-1}$ of synthetic air ($20 \text{ vol.}\% \text{ O}_2 + 80 \text{ vol.}\% \text{ N}_2$) containing 300–400 ppm of benzene was fed into the catalyst bed, corresponding to a space velocity of $\sim 120 \text{ L}\cdot\text{g}^{-1}\cdot\text{h}^{-1}$. After the adsorption-desorption-reaction equilibrium of benzene was achieved at one temperature on the catalyst surface, the catalyst was heated up with a rate of $5^\circ\text{C}\cdot\text{min}^{-1}$ to the next set temperature. Water vapor was generated by flowing synthetic air through a water bubbler at 26°C , and the humid air was then mixed with the dry air flow containing benzene. The outlet benzene concentration was monitored online by VOCs detector (MiniRAE 3000, USA), and benzene conversion was calculated according to the difference between the inlet and outlet benzene concentrations.

2.3. Temperature programmed desorption of adsorbed benzene (C_6H_6 -TPD), O_2 -TPD, surface oxidation reaction of benzene (C_6H_6 -SOR) and CO_2 -TPD

The interaction between benzene molecules and catalyst surface was evaluated by C_6H_6 -TPD. About 0.1 g of catalyst was used for C_6H_6 -TPD. $200 \text{ mL}\cdot\text{min}^{-1}$ of N_2 with $\sim 380 \text{ ppm}$ of benzene flowed through the catalyst bed. After adsorption for 1 h, $200 \text{ mL}\cdot\text{min}^{-1}$ of pure N_2 was switched into the reactor to purge the physically absorbed benzene molecules, and then the sample was heated at a rate of $10^\circ\text{C}\cdot\text{min}^{-1}$ to 400°C in the same atmosphere. The desorbed benzene was detected by the VOCs detector.

O_2 -TPD is useful to quantify the relative amounts of surface oxygen species and characterize their activities. O_2 -TPD was performed on Chemisorption Analyzer (Autochem II 2920, Micromeritics, USA). After pretreated in $50 \text{ mL}\cdot\text{min}^{-1}$ of helium at 105°C for 30 min and then cooled down to 40°C , the $\sim 0.05 \text{ g}$ of catalyst was subject to 30-min O_2 adsorption with $50 \text{ mL}\cdot\text{min}^{-1}$ of $5 \text{ vol.}\% \text{ O}_2/\text{He}$. After purged by $50 \text{ mL}\cdot\text{min}^{-1}$ of helium for 30 min to desorb the physisorbed O_2 , the catalyst was heated in the same atmosphere with a ramp of $10^\circ\text{C}\cdot\text{min}^{-1}$. The impurities were removed by a cold trap at -80°C before the outlet flow entered the thermal conductivity detector.

The C_6H_6 -SOR was adopted to assess the activity of the catalyst surface to activate gaseous oxygen for benzene oxidation. The dynamic switching between air and benzene was carried out as follows: first, the catalyst was activated in $100 \text{ mL}\cdot\text{min}^{-1}$ of synthetic air at 350°C or 200°C for 30 min; then, $200 \text{ mL}\cdot\text{min}^{-1}$ of N_2 with $\sim 380 \text{ ppm}$ of benzene was led into the reactor to initiate benzene oxidation by surface oxygen species. These procedures were repeated several times. The outlet benzene was monitored by the VOCs detector.

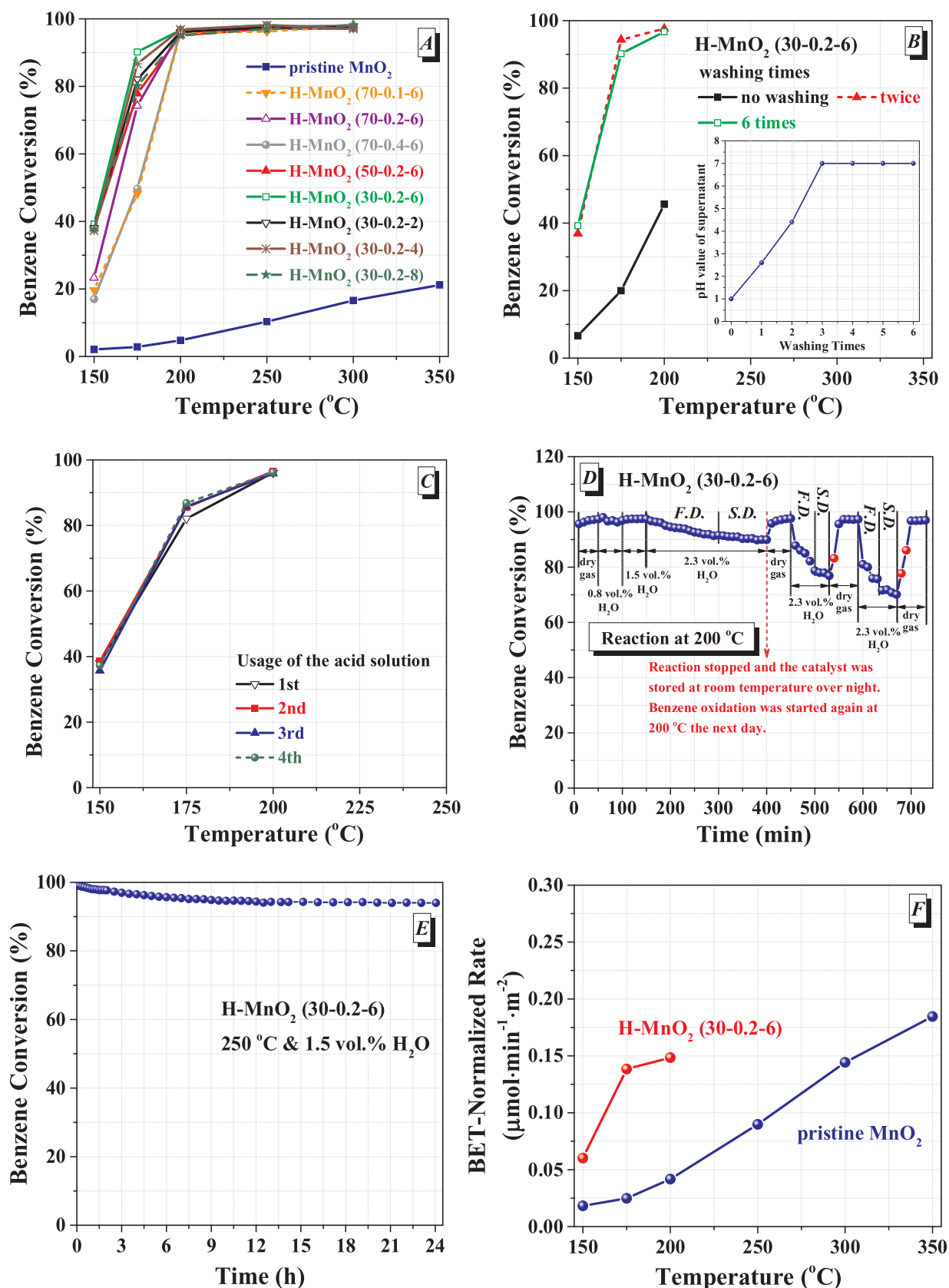


Fig. 1. (A) Temperature profiles of benzene conversion over the pristine and acid-treated MnO₂, (B) Effect of washing times on benzene oxidation over the H-MnO₂ (30-0.2-6) catalyst, (C) Comparison of benzene oxidation over the samples prepared by the recycled acid solutions, (D) Effect of humidity on benzene oxidation over the H-MnO₂ (30-0.2-6) catalyst at 200 °C, (E) Durability of the H-MnO₂ (30-0.2-6) catalyst for long-term reaction at 250 °C under 1.5 vol.% H₂O and (F) BET-normalized reaction rates of the pristine MnO₂ and H-MnO₂ (30-0.2-6). Inset in (B) shows the changes of the pH value of supernatant with washing times. Benzene oxidation conditions: 0.1 g of catalyst, 200 mL·min⁻¹ of synthetic air with 300–400 ppm of benzene.

CO₂-TPD was used to measure the interaction of benzene oxidation product with catalyst surface. The conditions of CO₂-TPD were similar to those of O₂-TPD except that 5 vol.% O₂/He was changed to pure CO₂ gas during adsorption stage.

3. Results and discussion

3.1. Activity tests

3.1.1. The optimal treatment conditions of birnessite MnO₂

Catalytic benzene oxidation over the pristine MnO₂ or H-MnO₂ obtained via different treatment conditions is comparatively shown in Fig. 1A to screen the optimal parameters of acid treatment, which clearly indicates that HNO₃ treatment remarkably enhanced benzene oxidation activity of birnessite MnO₂. When reaction temperature was lower than 200 °C, the pristine MnO₂ was almost inactive toward benzene oxidation with only 5% of benzene degraded at 200 °C and ~20% at an even higher temperature of 350 °C. After the pristine MnO₂ was treated with HNO₃, almost complete removal of benzene could be achieved at 200 °C with ~97% of removal efficiency regardless of the acid treatment conditions.

Moreover, it is also proposed from Fig. 1A that a proper combination of HNO₃ aqueous concentration, treatment temperature and treatment period is essential for the high activity of the H-MnO₂ catalysts. As to the HNO₃ aqueous concentration, it had an optimal value, neither too low nor too high. Treatment in 0.2 M of HNO₃ solution resulted in relatively better benzene oxidation performance, as seen from the comparison among H-MnO₂ (70-0.1-6), H-MnO₂ (70-0.2-6) and H-MnO₂ (70-0.4-6). Acid treatment at high temperature was not conducive to benzene oxidation since the benzene oxidation activity decreased in the sequence of H-MnO₂ (30-0.2-6) > H-MnO₂ (50-0.2-6) > H-MnO₂ (70-0.2-6). Four acid treatment periods (2 h, 4 h, 6 h and 8 h) were evaluated in this study and the changes of benzene conversion with the period of acid treatment exhibited volcano shape with 6 h being the optimal treatment time when the HNO₃ concentration and treatment temperature were fixed at 0.2 M and 30 °C, respectively. In particular, when the pristine MnO₂ was treated in 0.2 M of HNO₃ aqueous solution at 30 °C for 6 h, the as-obtained H-MnO₂ (30-0.2-6) catalyst possessed the highest activity, exhibiting ~40%, ~90% and ~97% of removal efficiency for 395 ppm of benzene under 120 L g⁻¹ h⁻¹ of space velocity at 150 °C, 175 °C and 200 °C, respectively. The CO₂ yield (%) was defined as the concentration ratio of formed CO₂ to the inlet benzene. The CO₂ yields of the catalysts at the reaction temperature of 175 °C are shown in Fig. S1. There was no CO₂ formed over the pristine MnO₂, and except the H-MnO₂ (30-0.2-6), the CO₂ yields of the other acid-treated samples were less than the corresponding benzene conversions to different extents, indicating the formation of oxidation by-products over these samples. The CO₂ yield of the H-MnO₂ (30-0.2-6) was almost the same as the corresponding benzene conversion (Fig. 1A), demonstrating its good mineralization rate. Therefore, the H-MnO₂ (30-0.2-6) catalyst was used for further study in the following sections. In our previous study [28], the T₅₀ and T₉₀ (corresponding to the respective reaction temperatures at which 50% and 90% of benzene conversions could be obtained) of the prepared Cu-modified birnessite MnO₂ were 193 °C and 240 °C, respectively, which were superior over the reported birnessite samples and were comparable to the noble metal catalysts in literature. As shown in Fig. 1A, the T₅₀ and T₉₀ of the H-MnO₂ (30-0.2-6) were 155 °C and 175 °C, respectively, obviously lower than those of the Cu-modified birnessite MnO₂, thereby paving road for the preparation of active benzene decomposition catalysts with potential for real-world application in the future.

3.1.2. Effect of washing times

Although the water washing process is critical during catalyst preparation, it consumes a large amount of water in mass production of solid materials. In view of the lack of fresh water resources in China, the

effect of washing times after acid treatment and centrifugal separation on benzene oxidation activity of the H-MnO₂ (30-0.2-6) was examined in this study. Dependence of benzene conversion on washing times is plotted in Fig. 1B. The pH value of the supernatant after each centrifugal separation increased with washing time and reached neutral after washing three times, as seen from the inset. Water washing is a compulsory step to render a high catalytic activity, testified by the greatly enhanced benzene conversion over the washed samples with respect to no washing, while there was no significant difference between washing twice and six times. As reported by Thevenet et al. [32], the existence of nitrate species (NO₃⁻) over the catalyst surface would block the active sites for acetaldehyde adsorption; besides, Lin et al. [33] found that N-containing intermediates, including nitrate, were accumulated on the catalyst surface during ozonation of NO, resulting in the occupation of the catalytically active sites. Therefore, in this study, the inferior activity of the catalyst without water washing in comparison with the thoroughly washed sample is likely due to the poisoning effect of NO₃⁻, which was deposited over the acid-treated surface during HNO₃ treatment. Thorough washing until the eluate becomes neutral is more easily controlled and more conducive to the reproducible production of the catalyst. Thus, washing six times was selected throughout this paper.

3.1.3. Reusability of the acid solution for GREEN process

As seen from the inset in Fig. 1B, the supernatant after the first centrifugal separation had a pH value of ~1.0, which was not allowed to be discharged directly without any treatment. Therefore, from the viewpoint of Green chemistry and recycling, it is important to investigate the reusability of the acid solution for multiple productions of catalysts. As shown in Fig. 1C, the activities of the H-MnO₂ samples prepared by the recycled acid solutions showed no decrease with respect to the sample prepared by the fresh acid solution, highlighting the feasibility of reusing the acid solution over times, and the synthetic strategy of birnessite material efficient for benzene oxidation by HNO₃ treatment thereby can be considered environmentally friendly.

3.1.4. Effects of humidity in feed gas and temperature fluctuation

As seen from the discussion above, the H-MnO₂ (30-0.2-6) sample is important for low-temperature removal of air benzene. However, the unavoidable moisture is not conducive to the desired reaction [34] and the water-resistant materials are very desirable. Therefore, the effect of humidity in feed gas on benzene oxidation over the H-MnO₂ (30-0.2-6) at 200 °C was then investigated. As shown in Fig. 1D, under the 0.8 vol.% and 1.5 vol.% of H₂O the catalyst did not show reduced activity with respect to the dry-gas reaction, all the three cases keeping ~97% of benzene conversion during the entire test. However, further increasing humidity to 2.3 vol.% resulted in gradual deactivation of the catalyst, and the benzene conversion was finally maintained around 90% after 4 h reaction. After the above four-stage reactions (50 min each for dry reaction, 0.8 vol.% and 1.5 vol.% of H₂O, and then 4 h for 2.3 vol.% of H₂O), the feed gas was stopped and the catalyst was cooled down and stored at room temperature overnight. When benzene oxidation was started again at 200 °C in dry gas the next day with the formerly used catalyst, benzene conversion still could be stably kept around 97% as before, suggesting that the H-MnO₂ (30-0.2-6) catalyst could be repeatedly used after heating and cooling processes, which are often encountered during practical applications. Thereafter, the benzene removal rate was evaluated at alternative dry and humid conditions. When the catalyst was subject to humid air with 2.3 vol.% of H₂O again, much faster and severer deactivation was observed with benzene conversion dropping from ~97% to ~77% in 80 min. Whereas, benzene conversion could be recovered to ~97% if the water vapor was cut off, but the recovery rate was slower than the latest cycle, as indicated by the number of the red data point, 10 min each. Most importantly, once the H₂O content returned to 2.3 vol.%, benzene conversion was quickly reduced to the level worse than the latest cycle, indicating that the

effect of water vapor was accumulated and did not disappear after treated in dry gas flow. As far as we know, there are different water-induced deactivation mechanisms for catalytic VOCs oxidation reported in literature. Chen et al. [35] reported that the oxidation of toluene followed a series of steps (toluene→intermediate→CO₂), and the intermediate→CO₂ step consumed more oxygen. Therefore, the decreasing oxygen concentration by introducing water was more negative to the transformation of intermediates to CO₂, resulting in the accumulation of oxidation byproducts over the catalyst surface and finally catalyst deactivation. On the other hand, the activity inhibition by water vapor is also likely to be the result of the competitive adsorption of water with benzene as well as oxygen molecules [34], which decreased the number of the catalytically active sites available for benzene oxidation. From Fig. 1D, it can be seen that when 2.3 vol.% of humidity was introduced into the feed gas, fast deactivation (F.D.) followed by slow deactivation (S.D.) was observed. Based on the discussion above, we think that the initial fast deactivation is due to the occupation of catalytically active sites by water molecules and the later slow deactivation is resulted from the gradual accumulation of surface intermediates.

3.1.5. Long-term stability in humid stream with 1.5 vol.% H₂O

The stability of the H-MnO₂ (30-0.2-6) catalyst for long-term oxidation of gaseous benzene was further tested. As shown in Fig. 1E, only a slight deactivation was observed in the first few hours and the H-MnO₂ (30-0.2-6) catalyst showed excellent stability during 24-h continuous test, keeping a stable removal efficiency of ~94% for 318 ppm of benzene under a high space velocity of 120 L·g⁻¹·h⁻¹ and 1.5 vol.% of H₂O at 250 °C.

Notably, as shown in Table 1, except the two samples tested under the very high humidities (3.6 vol.% and 7.2 vol.%), which are too high for our activity evaluation system to realize, the excellent water-resistant property of the H-MnO₂ (30-0.2-6) is better than those of the reported materials, even though the space velocity (60 L·g⁻¹·h⁻¹) adopted in these cases was only half the value adopted in this study (120 L·g⁻¹·h⁻¹). Thus, the H-MnO₂ (30-0.2-6) catalyst used in this study is a potential candidate for the remediation of benzene pollution from real air.

In the next section, the properties of the H-MnO₂ (30-0.2-6) were comparatively studied with the pristine MnO₂ through various characterizations and deliberately designed experiments to elucidate the

underlying mechanism for the promoting effect of acid treatment on benzene oxidation.

3.2. Characterization studies

3.2.1. Crystal structure, morphological changes and surface elements

XRD patterns of the pristine MnO₂ and H-MnO₂ (30-0.2-6) are displayed in Fig. 2A. The diffraction peaks around 12.0° {001}, 25.2° {002}, 37.6° {-111}, 42.3° {-112} and 66.5° {005} were observed over the pristine sample, which are well indexed to the standard information of birnessite MnO₂ (JCPDS 80-1098) without detectable impurity peaks, testifying the formation of layered structure but with poor crystallinity. It is also found that no phase changes occurred after acid treatment, although the relative intensities are slightly different. This could be ascribed to the partial destabilization of the layered structure from the leaching of K⁺ cations [40] by H⁺ ions in HNO₃, which will be discussed in the following EDS mapping and XPS measurements. Even after heat treatment at 200 °C and 300 °C for 3 h, the poor birnessite crystal structure was still retained, as shown in Fig. S2, indicating the good thermal stability of the catalysts. Thus, the influence of the changes of crystal structure on the catalytic performance in Fig. 1A could be excluded.

Morphological changes of the birnessite MnO₂ before and after acid treatment were studied by SEM. As shown in Fig. 2(B-1), the pristine MnO₂ (left image) was mainly present in compact layered structure, which is in accordance with the XRD result (Fig. 1A); however, this kind of compact morphology was significantly alleviated after acid treatment (right image), thus leading to the dramatic increase in S_{BET} (from 40 m²·g⁻¹ to 230 m²·g⁻¹), which played an important role in enhancing the contact efficiency between gaseous reactants and catalyst surface. Some of the layered structure was transformed into rods over the H-MnO₂ (30-0.2-6) catalyst, as pointed by the green arrows. K⁺ usually acts as layer adhesive, so the loss of K⁺ by H⁺ leaching, as evidenced by the following EDS mapping and K 2p XPS spectra, would cause destabilization of the layered structure [23,41], resulting in the smaller particle size. Considering the marked difference in BET surface areas of the pristine and acid-treated samples, the activities obtained from Fig. 1A could not reflect the intrinsic activities. Therefore, the normalized specific activities of the pristine MnO₂ and H-MnO₂ (30-0.2-6) to their BET surface areas were calculated since the BET surface area has been widely employed for metal oxide catalyst comparison [42]. As

Table 1
Summary of the reported data on catalytic oxidation of gaseous benzene in humid stream.

Sample	Preparation	Test conditions	X (T) ^a	Ref.
Mixture of Mn ₂ O ₃ and Mn ₃ O ₄	Reaction between (NH ₄) ₂ C ₂ O ₄ and Mn ²⁺ followed by 450 °C calcination	500 ppm C ₆ H ₆ /air 1.56 vol.% H ₂ O 60 L·g ⁻¹ ·h ⁻¹	47% (200 °C) 97% (250 °C)	[34]
Cu _{0.5} Co _{2.5} Al	Co-precipitation of Cu ²⁺ , Co ²⁺ and Al ³⁺ with Na ₂ CO ₃ followed by 400 °C calcination	500 ppm C ₆ H ₆ /air 1.5 vol.% H ₂ O 60 L·g ⁻¹ ·h ⁻¹	92% (320 °C)	[36]
Cu _{0.6} Mn	Nanocasting synthesis with mole ratio of Cu/Mn = 0.6	500 ppm C ₆ H ₆ /air 1.5 vol.% H ₂ O 60 L·g ⁻¹ ·h ⁻¹	90% (260 °C)	[37]
CoMn ₂ AlO-550	Co-precipitation of Co ²⁺ , Mn ²⁺ and Al ³⁺ with NH ₄ OH followed by hydrothermal treatment and 550 °C calcination	100 ppm C ₆ H ₆ /air 7.2 vol.% H ₂ O ^b 60 L·g ⁻¹ ·h ⁻¹	40% (190 °C) 100% (230 °C)	[38]
Co ^{II} Co ^{III} layered double hydroxide	Mixed stirring Co(NO ₃) ₂ with ammoniacal nitrogen followed by 400 °C calcination	100 ppm C ₆ H ₆ /air 3.6 vol.% H ₂ O ^b 60 L·g ⁻¹ ·h ⁻¹	98% (230 °C)	[39]
Cu modified birnessite	Redox between KMnO ₄ and Mn ²⁺ followed by Cu ²⁺ exchange	314 ppm C ₆ H ₆ /air 1.5 vol.% H ₂ O 120 L·g ⁻¹ ·h ⁻¹	90% (300 °C)	[28]
H-MnO ₂	Redox between KMnO ₄ and CH ₃ OH solution followed by HNO ₃ treatment	318 ppm C ₆ H ₆ /air 1.5 vol.% H ₂ O 120 L·g ⁻¹ ·h ⁻¹	57% (200 °C) 94% (250 °C)	This work

^a X (T) represents benzene conversion (X) at a specific reaction temperature (T).

^b These two humidities are too high for our activity evaluation system to realize at the time of submission.

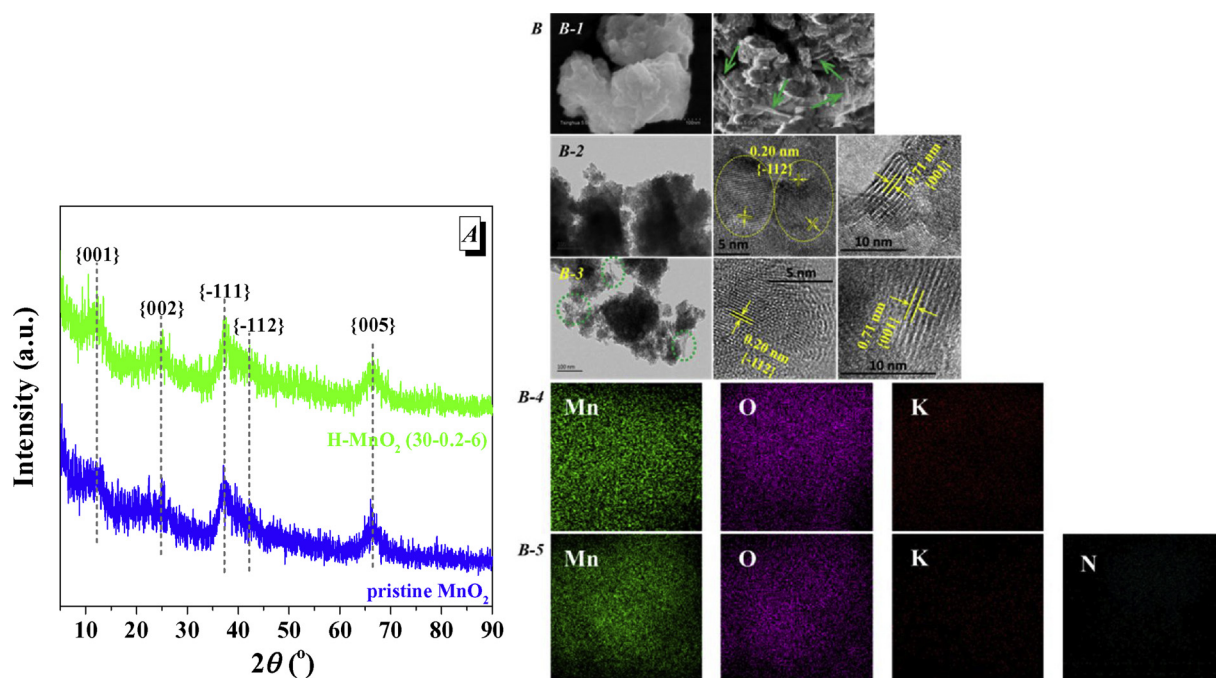


Fig. 2. (A) XRD patterns and (B) SEM & (HR)TEM images and EDS elemental maps of the catalysts. The left image in B-1 and Images B-2 & B-4 represent the pristine MnO_2 ; the right image in B-1 and Images B-3 & B-5 represent the H-MnO_2 (30-0.2-6).

exhibited in Fig. 1F, the H-MnO_2 (30-0.2-6) outperformed the pristine MnO_2 with much higher specific reaction rates, demonstrating the excellent intrinsic reactivity of the reaction sites over the H-MnO_2 (30-0.2-6).

The (HR)TEM images of the pristine MnO_2 and H-MnO_2 (30-0.2-6) are exhibited in Fig. 2(B-2) and (B-3), respectively. The layered structure was also observed by TEM over both samples, and rods were detected over the H-MnO_2 (30-0.2-6) circled by green dashes, which agrees well with the above SEM observations. In addition, it is found that acid treatment had little effect on the exposed facets and both samples exposed the typical crystal planes of birnessite MnO_2 , which was confirmed in many areas throughout the sample (not all the HRTEM photos were given in this study). However, the sharpness of the lattice fringes before and after acid treatment was very different, and the lattice fringes of the H-MnO_2 (30-0.2-6) became blurred compared with the pristine MnO_2 , as manifested by the comparative observation of the $\{-112\}$ and $\{001\}$ planes of the two samples. This result suggests that the formation of crystal defect by acid treatment caused distortion to the ordered lattice structure of the birnessite MnO_2 . To investigate the composition distributions, the EDS mapping images were taken, which show that Mn and O were evenly distributed over both samples (Fig. 2(B-4) and (B-5) before and after acid treatment, respectively). The K signal of the H-MnO_2 (30-0.2-6) was much weaker than that of the pristine MnO_2 as a result of K^+ replacement by H^+ exchange. The existence of H^+ in the acid-treated birnessite MnO_2 was supported by the H^1 -NMR characterization in our previous study [23]. No residual N element was detected over the H-MnO_2 (30-0.2-6) probably due to the thorough washing after acid treatment.

The effects of crystal structure and exposed facet on benzene oxidation activity thereby could be ruled out as evidenced by the above XRD and HRTEM results. Considering that catalytic activity is highly related to the surface electronic structure, the role of the oxidation state of surface elements in determining the benzene oxidation performance was then investigated by XPS, with the results depicted in Fig. 3. The empirical relationship between the average oxidation state (AOS) of surface Mn atoms and the Mn 3s multiplet energy (ΔE) is useful and reliable to estimate the chemical valence of Mn element since the binding energies of different Mn valences in Mn 2p spectra are close to

each other [43], thus making it difficult to fulfill objective and definite deconvolutions. Substitute the values of ΔE s in Fig. 3A into the formula of $\text{AOS} = 9.27 - 1.18 \times \Delta E$ [44], and the AOSs of Mn were worked out. As listed in Table 2, the AOS of Mn over the H-MnO_2 (30-0.2-6) surface was ~ 3.5 , lower than that of the pristine MnO_2 by 0.2. The lower Mn valence resulted from acid treatment was also confirmed by the Mn 2p results, shown in Fig. 3B. Two peaks, centered at ~ 653.0 eV and ~ 641.0 eV, were observed over both samples, corresponding to the Mn $2p_{1/2}$ and Mn $2p_{3/2}$, respectively [45]. Notably, the Mn 2p peaks of the H-MnO_2 (30-0.2-6) shifted to lower binding energies compared with those of the pristine MnO_2 , proving the increased surface electron density after acid treatment. As a result, the valence of the surface Mn decreased over the acid-treated sample. For charge balance, the reduced positive charges thereby will be neutralized by less negatively charged species, e.g., O^{2-} , which will induce the formation of oxygen vacancies. Therefore, the H-MnO_2 (30-0.2-6) possessed more oxygen vacancies than the pristine sample. Multiple O 1s peaks were observed for both samples (Fig. 3C), indicating the existence of surface oxygen species having varied chemical environments. According to literature [46], the O 1s peaks from low to high binding energies could be assigned to the oxygen species from lattice oxygen (O_{lat}) and surface adsorbed oxygen (O_{ads}). Also as shown in Table 2, the H-MnO_2 (30-0.2-6) had higher surface $\text{O}_{\text{ads}}/\text{O}_{\text{total}}$ ratio ($= 0.45$) with respect to the pristine MnO_2 ($= 0.23$), testifying the generation of more surface active oxygen sites by acid treatment. What is more, the surface adsorbed oxygen content can reflect the amount of surface oxygen vacancies on the basis of the concept that oxygen molecules are usually adsorbed on the oxygen vacancy sites over metal oxides [47]. Apparently, the higher $\text{O}_{\text{ads}}/\text{O}_{\text{total}}$ ratio of the H-MnO_2 (30-0.2-6) signifies its larger amount of oxygen vacancies, consistent with the Mn 3s data that acid treatment of birnessite MnO_2 contributed to the formation of oxygen vacancies. The K 2p spectra of the catalysts before and after acid treatment are displayed in Fig. 3D. The K signal was dramatically weakened over the H-MnO_2 (30-0.2-6), meaning the loss of K^+ ions due to the leaching effect of H^+ exchange during acid treatment. This result agrees well with the elemental distributions in Fig. 2B.

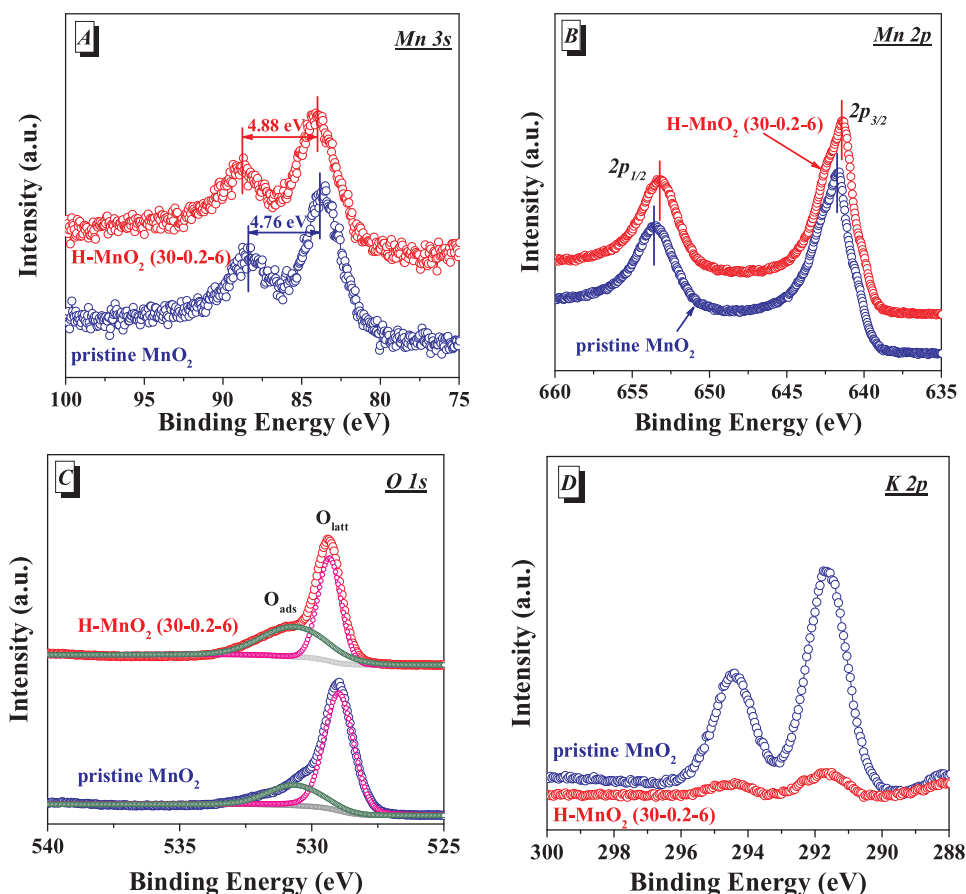


Fig. 3. XPS spectra of the catalysts.

Table 2
Summary of the XPS results.

Sample	AOS of Mn	$O_{\text{ads}} / O_{\text{total}}$
pristine MnO_2	3.7	0.23
H- MnO_2 (30-0.2-6)	3.5	0.45

3.2.2. Redox behavior and surface acidity

H_2 -TPR is a good method to evaluate the redox properties of solid materials, which can be correlated with their catalytic performances for oxidation reactions [48]. Chen et al. [49,50] reported that the good reducibility of the metal oxide catalysts was conducive to the improved performance for toluene oxidation. The H_2 -TPR results of the pristine MnO_2 and H- MnO_2 (30-0.2-6) are shown in Fig. 4A. For the pristine MnO_2 , the reduction mainly occurred from 300 °C to 400 °C with a small reduction peak around 250 °C, denoted as O_{β} and O_{α} , respectively. According to the Mn 3s XPS results, the Mn AOS of the pristine MnO_2 was about 3.7 (Table 2), suggesting that Mn mainly existed as mixture of Mn^{3+} and Mn^{4+} . Thus, at a first glance, these two peaks belong to the continuous reductions of manganese oxide, which, however, is not the case. Based on the deconvolution and integration results, the peak area ratio of O_{α} to O_{β} was about 4:13, which is quite different from the theoretical value of 7:13 obtained from the consecutive reductions of MnO_2 to Mn_2O_3 to MnO and the fact that the atomic ratio of Mn^{3+} to Mn^{4+} over the pristine MnO_2 was 3:7 according to its Mn AOS. In addition, the peak area ratio of O_{α} to ($O_{\alpha} + O_{\beta}$) was 0.24, very close to the content of surface adsorbed oxygen over the pristine MnO_2 (= 0.23, Table 2). It is thereby reasonable to deduce that the O_{α} and O_{β} peaks in the H_2 -TPR profile of the pristine MnO_2 are assigned to the respective reductions of the oxygen species from surface adsorbed oxygen and MnO_x lattice. After acid treatment,

significant changes happened to the redox behavior of the birnessite MnO_2 , mainly in the low-temperature range (< 300 °C). In addition to the H_2 consumption peak near 250 °C (O_{α}), another strong and sharp reduction peak was detected at 293 °C. The peak area ratio of O_{α} to the total oxygen species was 0.41, almost the same as the content of surface adsorbed oxygen over the H- MnO_2 (30-0.2-6) (= 0.45, Table 2), further confirming that the O_{α} peak belongs to the reduction of surface adsorbed oxygen. The starting reduction temperature of O_{α} was 113 °C over the H- MnO_2 (30-0.2-6), much lower than that over the pristine MnO_2 (= 136 °C), as seen in the inset, demonstrating that acid treatment increased the activity of surface adsorbed oxygen, thus lowering the reduction temperature. Additionally, the 293 °C and 360 °C peaks over the H- MnO_2 (30-0.2-6) are tentatively attributed to the consecutive reductions of the MnO_x lattice oxygen (O_{β}). However, the peak area ratio of these two peaks was calculated to be about 1:1, which is larger than theoretical value of 1:3 based on the consecutive reductions of MnO_2 to Mn_2O_3 to MnO and the fact that the atomic ratio of Mn^{3+} to Mn^{4+} was 1:1 according to the Mn AOS of 3.5. The plausible explanation might be that the lattice oxygen became more facile and reducible because of acid treatment, thus resulting in the early reduction.

The changes of surface acidity of the birnessite MnO_2 after acid treatment were assessed by pyridine adsorbed IR spectroscopy to determine the nature and obtain the amounts of the acid sites between Lewis-acid sites (L-sites) and Brønsted-acid sites (B-sites). As reported by Wu et al. [51], the L-sites act as the core active sites for the cleavage of the C–C bands in the benzene ring, which is important to the complete oxidation of benzene. The pyridine-IR spectra of the pristine MnO_2 and H- MnO_2 (30-0.2-6) at 40 °C, 100 °C and 200 °C are shown in Fig. 4B. According to the literature [51], the peak assignments were as follows: the peak at 1540 cm^{-1} is attributed to pyridine adsorbed on B-sites, and bands at 1610 cm^{-1} and 1450 cm^{-1} are due to pyridine

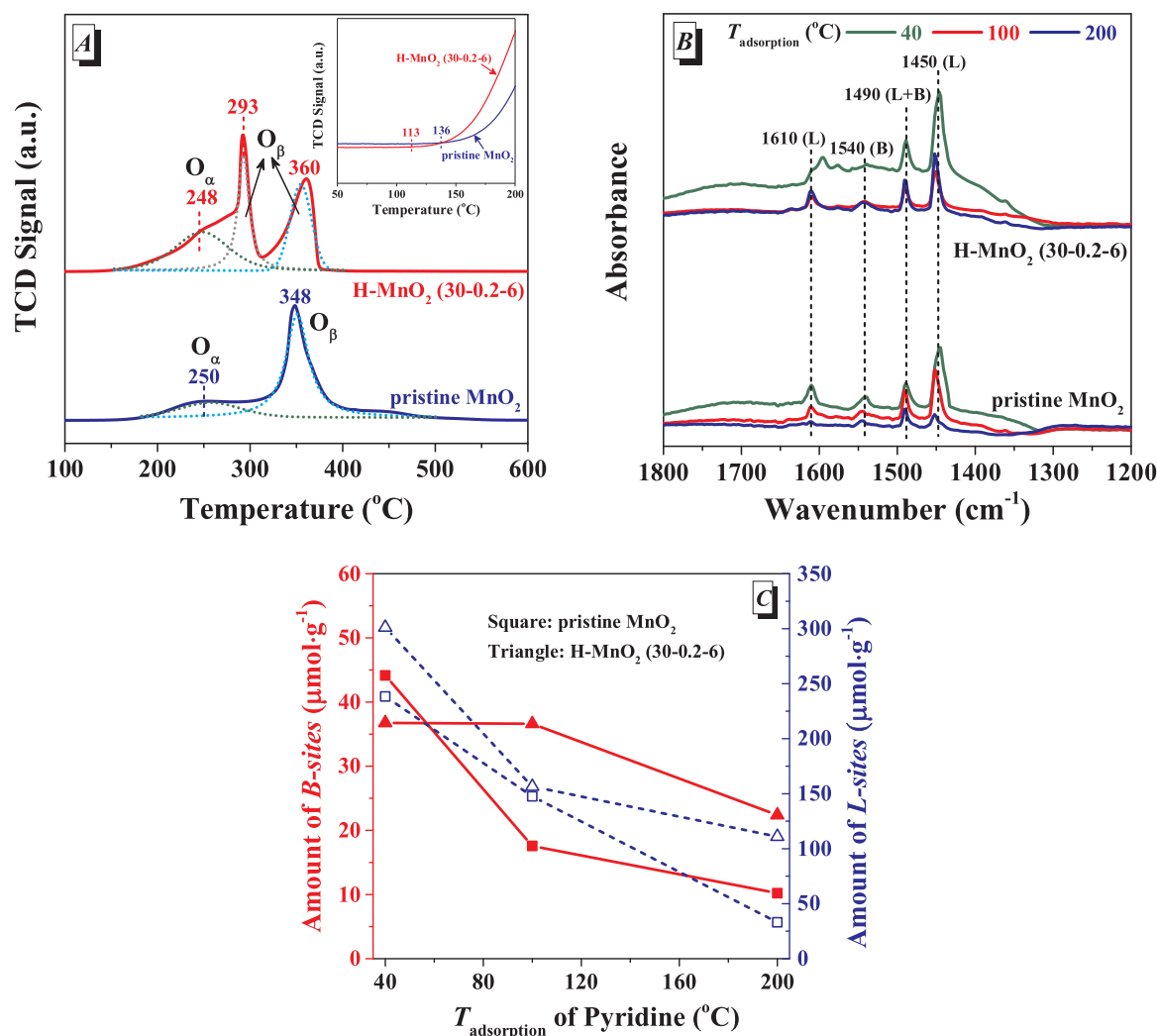


Fig. 4. (A) H₂-TPR profiles of the catalysts, (B) Pyridine-IR spectra of the pristine MnO₂ and H-MnO₂ (30-0.2-6) at 40 °C (—), 100 °C (—) and 200 °C (—), and (C) Amounts of the Lewis-acid sites and Brønsted-acid sites over these two samples plotted against the adsorption temperature of pyridine. H₂-TPR conditions: 0.05 g of catalyst, 50 mL·min⁻¹ of 5 vol.% H₂/Ar, 10 °C·min⁻¹.

adsorbed on L-sites; the band at 1490 cm⁻¹ is resulted from pyridine adsorbed on both L-sites and B-sites. The peak intensities decreased as the catalyst was heated to higher temperatures due to the desorption of pyridine adsorbed on weak acid sites, but the decreasing extent was quite different between the pristine and acid-treated samples. In this study, the adsorbed pyridine at 200 °C was used to assess the amount of strong acid sites, and the adsorbed pyridine at 40 °C was used to calculate the total amount of acid sites. For clarity, the amounts of the L-sites and B-sites over these two samples are plotted against the adsorption temperature of pyridine in Fig. 4C, which manifests that the L-sites dominated over the B-sites for both samples at all three adsorption temperatures and the acid-treated surface could provide more acid sites, including the strong B- and L-sites, than the pristine MnO₂. The larger amount of acid sites and the stronger acidity of the H-MnO₂ (30-0.2-6) might also facilitate benzene oxidation [51,52].

3.2.3. Interaction of reactants and products with catalyst and activation of reactant molecules

3.2.3.1. Interaction and activation of benzene with catalysts. Benzene adsorption and then desorption in N₂ (C₆H₆-TPD) was used to study the interaction and activation of benzene molecules with catalyst surface. As shown in Fig. 5A, at benzene adsorption stage, the outlet benzene concentration did not change too much when the benzene feed gas flowed through the pristine MnO₂ whereas it decreased to a much

lower value over the H-MnO₂ (30-0.2-6), substantiating the higher adsorption capacity of benzene induced by acid treatment. During N₂ purging (benzene was cut off), which was used to desorb the physisorbed benzene, for the pristine MnO₂, the outlet benzene concentration decreased fast to nearly 15 ppm in ~1 h, which, however, dropped much more slowly over the H-MnO₂ (30-0.2-6), and about 40 ppm of benzene could still be detected even after ~3-h purging. When the catalyst covered with benzene was heated with a rate of 10 °C·min⁻¹ in N₂, benzene desorption peaks centered at 90 °C and 100 °C were detected over the pristine MnO₂ and H-MnO₂ (30-0.2-6), respectively, and more benzene was evolved from the H-MnO₂ (30-0.2-6), inferred from its larger desorption peak, corresponding to 12.3 mmol_{C₆H₆}·g_{cat}⁻¹ vs. 4.9 mmol_{C₆H₆}·g_{cat}⁻¹ by integrating the desorption curves. Besides, another benzene evolution peak was observed at a much higher temperature of 330 °C over the H-MnO₂ (30-0.2-6), as shown in the inset, which, however, was not found over the pristine sample. Wan and co-authors [53] carried out C₆H₆-TPD measurement over the composites of Fe, Mn and Zr, and benzene evolution occurred at an even higher temperature of 570 °C, which is ascribed to the benzene desorption from catalyst surface. Therefore, in this study, the benzene evolution peak at 330 °C can be ascribed to the benzene desorption from catalyst surface, not due to the re-polymerization of the byproducts during benzene decomposition. The larger adsorption capacity of benzene together with the higher desorption temperatures

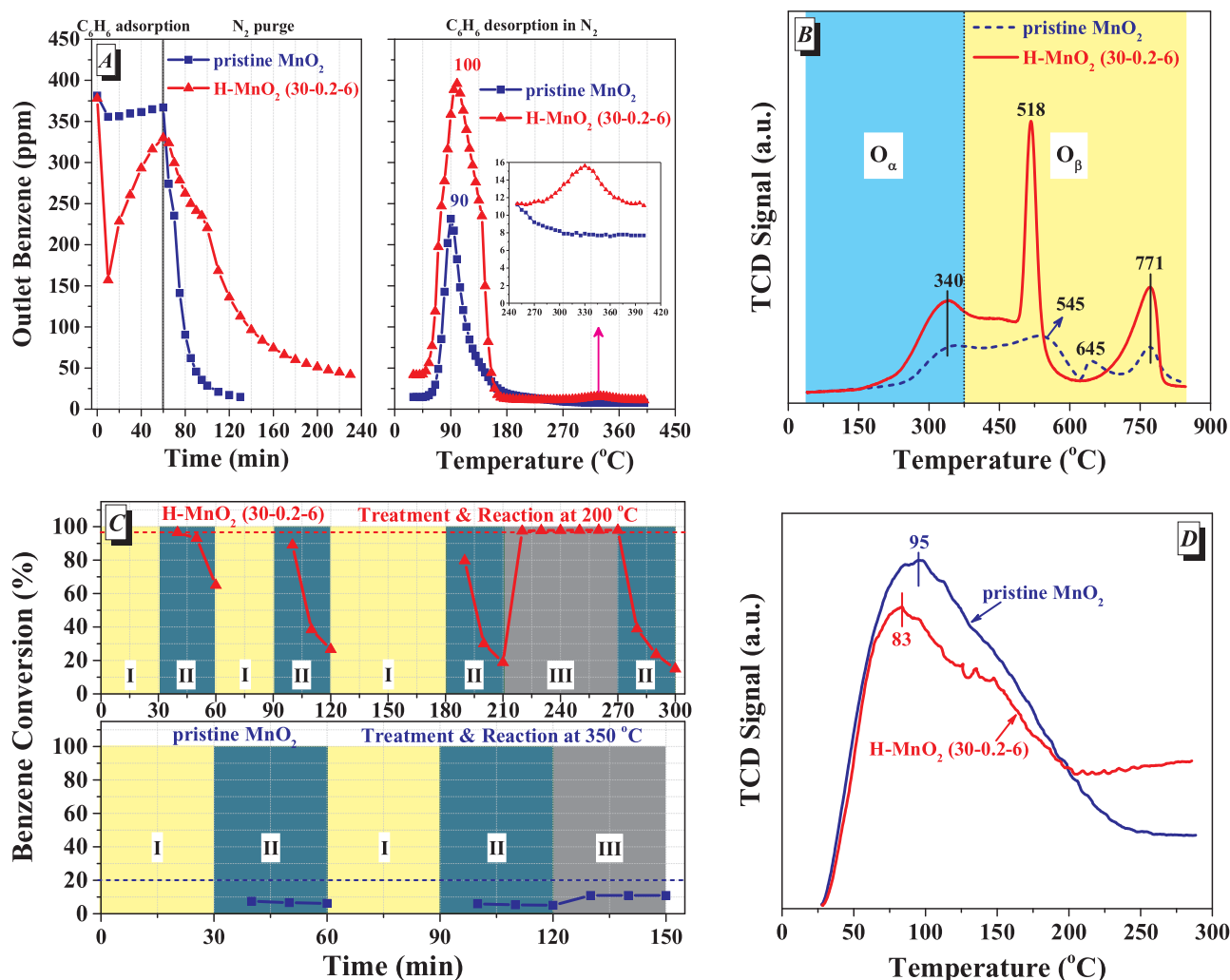


Fig. 5. (A) C₆H₆-TPD, (B) O₂-TPD, (C) C₆H₆-SOR and (D) CO₂-TPD of the catalysts. For C₆H₆-TPD: ~0.1 g of catalyst, 200 mL·min⁻¹ of N₂ with ~380 ppm of benzene for 1 h adsorption, room temperature; 200 mL·min⁻¹ of pure N₂ for desorption, 10 °C·min⁻¹. For O₂-TPD: ~0.05 g of catalyst, 50 mL·min⁻¹ of 5 vol.% O₂/He for 30-min adsorption, room temperature; 50 mL·min⁻¹ of helium for desorption, 10 °C·min⁻¹. Reaction conditions for Zone (I), (II) and (III) in (C) are as follows: treatment in 100 mL·min⁻¹ of synthetic air; 200 mL·min⁻¹ of N₂ containing ~380 ppm of benzene; 200 mL·min⁻¹ of synthetic air containing ~380 ppm of benzene, and the treatment and reaction temperatures were 350 °C and 200 °C for the pristine MnO₂ and H-MnO₂ (30-0.2-6), respectively. The conditions of CO₂-TPD were similar to those of O₂-TPD except that 5 vol.% O₂/He was changed to pure CO₂ gas during adsorption stage.

of adsorbed benzene over the H-MnO₂ (30-0.2-6) might be correlated with its larger amount of acid sites and stronger surface acidity (pyridine IR, Fig. 4B and C) since acid sites play an important role in the adsorption of hydrocarbons [52]. Conclusively, the much stronger affinity of gaseous benzene to the acid-treated surface would probably result in an easier activation of benzene molecules during benzene oxidation reaction.

3.2.3.2. Interaction and activation of oxygen with catalysts. Oxygen adsorption and then desorption in helium (O₂-TPD) was used to study the interaction and activation of oxygen molecules with catalyst surface, with the results shown in Fig. 5B. According to the literature [54], for both the pristine MnO₂ and H-MnO₂ (30-0.2-6), their O₂-TPD curves could be divided into two parts: the O₂ evolved at temperatures below 400 °C and higher than 400 °C are assigned to the release of surface adsorbed oxygen (O_α) and lattice oxygen (O_β), respectively. Although the surface adsorbed oxygen had the same desorption temperature (~340 °C) over both samples, acid treatment evidently increased the amount of surface adsorbed oxygen, judged from the larger desorption peak of O_α over the H-MnO₂ (30-0.2-6), which demonstrates that the acid-treated surface provided more sites, i.e.,

oxygen vacancies, to accommodate oxygen species. This is in accordance with the O 1s XPS (Fig. 3C) and H₂-TPR (Fig. 4A) measurements. In terms of lattice oxygen, the peak profiles and peak positions of the acid-treated sample have changed remarkably with respect to the pristine MnO₂. For the pristine MnO₂, three O_β peaks were observed at 545 °C, 645 °C and 771 °C, representing the stepwise desorption of the MnO₂ lattice oxygen, i.e., MnO₂ → Mn₂O₃ → Mn₃O₄ → MnO [55]. However, after acid treatment, the 545 °C and 645 °C peaks over the pristine MnO₂ were transformed into a strong and sharp peak at a much lower temperature of 518 °C over the H-MnO₂ (30-0.2-6), testifying to the generation of more active lattice oxygen by acid treatment. This is also in good accordance with the H₂-TPR results (Fig. 4A).

3.2.3.3. Surface oxidation reaction of benzene (C₆H₆-SOR). There is a definitive consensus in literature that the catalytic oxidation of VOCs proceeds through the Mars-van Krevelen mechanism [56]: the pollutant molecules first adsorb on the catalyst surface, followed by abstracting lattice oxygen species, the pollutant being oxidized and the catalyst being reduced with the formation of oxygen vacancies, which are later replenished by oxygen from gas phase for the next reaction cycle.

Herein, the C₆H₆-SOR was specially designed to further clarify the promoting effect of acid treatment on benzene oxidation. C₆H₆-SOR was conducted by alternating synthetic air (Zone I) and C₆H₆/N₂ (Zone II) through catalyst bed, as displayed in Fig. 5C. Zone I was used to supplement the surface oxygen species and Zone II was used to evaluate the reactivity of the surface oxygen species for benzene oxidation, thus reflecting the activity of surface active sites to activate the oxygen species. The C₆H₆-SOR was performed at 350 °C and 200 °C, respectively, over the pristine and acid-treated samples because of the high benzene removal efficiency obtained at the corresponding temperature (Fig. 1A).

For the H-MnO₂ (30-0.2-6), during the first “air treatment (Zone I) - benzene oxidation (Zone II)” cycle, benzene could be removed with high efficiency (~97%), equal to the value achieved by feeding the mixture of benzene and synthetic air into the catalyst (dashed line), in the initial 10 min due to the abundant surface oxygen species; then benzene conversion decreased gradually with reaction time due to the consumption of surface oxygen species; at the end of the first cycle, benzene conversion dropped to 65%. After the catalyst was purged with synthetic air at 200 °C for 30 min, the initial benzene conversion was only recovered to ~89% in the second cycle and decreased much faster than in the first cycle thereafter. Even if the catalyst was regenerated for 1 h in the third cycle, its benzene conversion still could not be fully recovered, which was lower than that of the second cycle (~79% vs. ~89%), but the decaying rate of benzene conversion seemed similar to that of the second cycle. According to Föttinger, Rupprechter and their coauthors [57], who performed CO vs. O₂ switching experiments over Co₃O₄, not only surface oxygen might take part in CO oxidation, but also oxygen from the bulk, and the reaction rate with surface oxygen was faster than with the bulk oxygen, which needs to diffuse to the surface to react with CO. Therefore, in this study, it is reasonable to infer that both surface and bulk oxygen participated in benzene oxidation during the first O₂ vs. benzene switching experiment while only surface oxygen was involved for the following cycles. That is because if only surface oxygen would react during the first cycle, then its benzene conversion should not have dropped less slowly than in the second and third cycles. The above results thus imply that the bulk oxygen was not so easily regenerated as the surface oxygen and the surface oxygen was the main active species for benzene oxidation in this study. When benzene and air simultaneously passed through the catalyst (Zone III), benzene conversion rapidly increased to ~97% and kept stable for 1 h owing to the continuous replenishment of the surface oxygen by oxygen from gas phase, followed by a rapid reduction once air was cut off again (the last Zone II). Another possibility for the deactivation phenomenon might be due to the accumulation of intermediates or coke deposition. The FT-IR spectrum of the used H-MnO₂ (30-0.2-6) after benzene oxidation at 150 °C for 4 h was collected, with the result displayed in Fig. S3, which demonstrates that new peaks due to the oxidation byproducts appeared over the used catalyst in comparison with the fresh sample.

In sharp contrast to the H-MnO₂ (30-0.2-6), the activity of the pristine MnO₂ to activate surface oxygen species was very poor with less than 10% of benzene being removed at 350 °C (Zone II). Even feeding the mixture of benzene and synthetic air together into the catalyst (Zone III) still could not recover the catalyst (lower than the dashed line). This is because the inert surface oxygen species, which were accumulated over the catalyst surface during the air treatment stage (Zone I), together with the deposition of reaction intermediates (as reflected from the FT-IR spectrum of the used pristine MnO₂ after benzene oxidation at 250 °C for 4 h in Fig. S3) occupied the catalytically active sites for reactions. Based on the discussions of O₂-TPD and C₆H₆-SOR, it can be concluded that compared with the pristine MnO₂, the acid-treated surface was much more reactive for the activation of surface oxygen species for benzene oxidation.

3.2.3.4. The desorption of oxidation products from catalysts. For catalytic reactions, the desorption of reaction products from catalyst surface is a

prerequisite for the regeneration of active sites for the next reaction cycle. Therefore, the easy desorption of products from the catalytically active sites is also important to realize a high and stable activity. As demonstrated by the FT-IR spectra of the used catalysts in Fig. S3, not only CO₂ but also other kinds of oxidation products were formed during benzene oxidation. In order to simplify the situation, in this study, the complete oxidation product of benzene, i.e., CO₂, was tentatively used as the probe molecule, and the TPD of adsorbed CO₂ from the pristine and acid-treated samples was performed to explain the high activity of the acid-treated MnO₂ from a new angle of product desorption, with the CO₂-TPD curves shown in Fig. 5D. O₂ desorption had negligible interference with the CO₂-TPD curves because nearly no O₂ was desorbed below 200 °C (O₂-TPD, Fig. 5B). Both samples exhibited a similar desorption contour of CO₂ from 30 °C to 200 °C, but the adsorbed CO₂ over the H-MnO₂ (30-0.2-6) was more easily desorbed than over the pristine MnO₂, as inferred from the lower desorption temperature (83 °C vs. 95 °C). Moreover, the pristine MnO₂ acted more like a CO₂ reservoir since more CO₂ was evolved from it, rationalized by its larger desorption peak. Based on the above discussion, the higher activity of the H-MnO₂ (30-0.2-6) for benzene oxidation was also related to its weaker interaction with the oxidation product, and the occupied active sites by oxidation products over the acid-treated surface were more easily regenerated.

3.3. Discussion on the tremendous effect of acid treatment on benzene oxidation

From a macroscopic point of view, acid treatment decreased the content of interlayer K⁺ cations of birnessite MnO₂ via H⁺ ion exchange (EDS mapping in Fig. 2B and K 2p XPS in Fig. 3D), which was also accompanied by many changes in microscopic properties. The discussion will be carried out mainly from the following two aspects: benzene activation by surface acid sites and oxygen vacancy promoted activation of surface oxygen.

3.3.1. Benzene activation

The adsorption capacity and binding strength of catalyst surface with pollutant molecules are crucial to the catalytic degradation of pollutants. Wang and coworkers [58] discovered that CO oxidation preferentially occurred over the surface that could provide abundant active sites for CO adsorption, to say, with larger CO adsorption capacity. Weaver et al. [59] investigated the intrinsic reactivity for CO oxidation on single-layer and multilayer PdO {101} grown on Pd {100}, and their DFT calculation results correlated the higher CO oxidation activity of multilayer sample with the stronger binding of CO on multilayer PdO {101}. In this study, benzene adsorption and then desorption in inert gas (C₆H₆-TPD, Fig. 5A) was designed to evaluate the capacity and strength of benzene adsorption on the catalysts. The acid-treated MnO₂ possessed much larger adsorption capacity for benzene, which was about 2.5 times that of the pristine MnO₂ (12.3 mmol_{C₆H₆}g_{cat}⁻¹ vs. 4.9 mmol_{C₆H₆}g_{cat}⁻¹). What is more, benzene molecules were more strongly bonded to the acid surface, supported by the higher desorption temperatures of benzene over the H-MnO₂ (30-0.2-6) (= 100 °C and 330 °C) than over the pristine MnO₂ (= 90 °C). As reported by other researchers [52,60], the preferential affinity of the acid-treated surface to benzene molecules might come from its abundant acid sites and strong acidity, especially the L-sites (pyridine-IR, Fig. 4B and C). The L-sites played an important role in the reactions following the Mars-van Krevelen mechanism, as reviewed by Corma and García [61]. The larger amount of benzene adsorption as well as the stronger binding strength of benzene molecules on the H-MnO₂ (30-0.2-6) facilitated the activation of benzene for the subsequent thermal oxidation.

3.3.2. Oxygen vacancy promoted activation of surface oxygen

Benzene oxidation on metal oxide catalysts generally goes through a

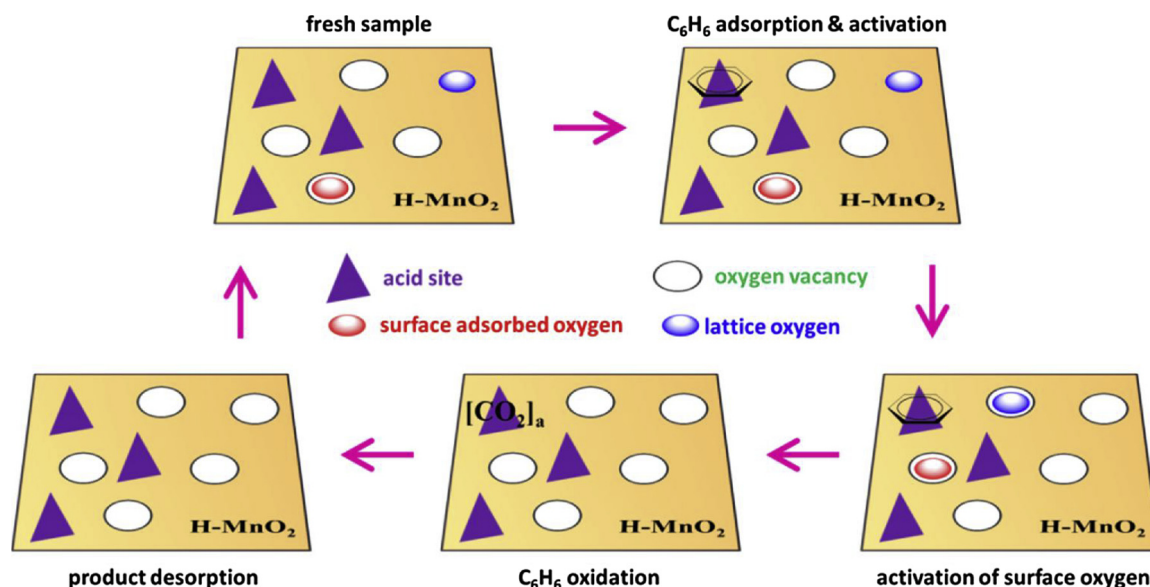


Fig. 6. Illustration of benzene oxidation over the H-MnO₂ (30-0.2-6).

Mars-van Krevelen mechanism, in which benzene molecules adsorb first on the catalyst surface and are activated, and then oxidized by lattice oxygen. Therefore, besides benzene activation, the activation of surface oxygen species is also crucial to catalytic benzene oxidation. Oxygen vacancy is considered as the active site for the activation of oxygen species. If the number of oxygen atoms is less than what is expected in a perfect crystal, it can be said that oxygen vacancies are formed. Li et al. [25] reported that the presence of oxygen vacancies in MnO₂ tremendously improved its catalytic activity for benzene oxidation. Wang et al. [62,63] also pointed out that the defective sites of oxygen on MnO₂ were beneficial to formaldehyde oxidation. Acid treatment of birnessite MnO₂ increased the number of oxygen vacancy, verified by the Mn 3s and O 1s XPS measurements (Fig. 3A and C). When it comes to the activity of surface oxygen species, on one hand, acid treatment promoted the mobility of lattice oxygen, as seen from the much lower reduction (H₂-TPR, Fig. 4A) and desorption (O₂-TPD, Fig. 5B) temperatures of the lattice oxygen over the H-MnO₂ (30-0.2-6); on the other hand, the surface adsorbed oxygen over the H-MnO₂ (30-0.2-6) also exhibited higher activity than over the pristine MnO₂, testified by the lower reduction temperature during H₂-TPR measurements. In our previous studies [30,44], it was found that the formation of active surface oxygen species was related to the activity of oxygen vacancies, i.e., the more active the oxygen vacancies are, the more facile and mobile the surface oxygen species will be, from which it can be deduced that compared with the pristine MnO₂, the acid-treated sample not only had more oxygen vacancies, but also possessed higher oxygen vacancy activity. The highly active lattice oxygen and surface adsorbed oxygen would react with the activated benzene molecules, which is supported by the C₆H₆-SOR experiments (Fig. 5C). Kim and Shim [14] investigated benzene and toluene combustion over a series of manganese oxides and they also correlated the catalytic activity with the oxygen mobility on the catalysts. Moreover, there existed an intrinsic relationship between oxygen vacancy and acid site, and both of them could be correlated with the Mn element. As discussed in the XPS characterization (Fig. 3), lower average oxidation state of Mn implies the formation of more oxygen vacancies, and the amount of oxygen vacancy is related to the Mn³⁺ content. In addition, oxygen vacancy itself is a kind of L-site [64], and oxygen vacancies may be occupied by water and its dissociative species, i.e., surface hydroxyl groups, which usually act as the potential B-sites.

Finally, the easy desorption of oxidation products (CO₂-TPD, Fig. 5D) resulted in a fast regeneration of the active sites. At this point,

one catalytic cycle over the H-MnO₂ (30-0.2-6) is closed. For clarity, the complete reaction cycle for benzene oxidation over the acid-treated surface is illustrated in Fig. 6.

In order to test the universality of the HNO₃ treatment method for other MnO₂ materials, β-MnO₂ (1 × 1 tunnel), α-MnO₂ (2 × 2 tunnel) and todorokite MnO₂ (3 × 3 tunnel) were prepared, treated by 0.2 M of HNO₃ solution at 30 °C for 6 h, and then used in benzene oxidation. Moreover, the commercial Aladdin MnO₂ (CAS: 1313-13-9) was also studied. The crystal structures of the as-prepared β-MnO₂, α-MnO₂ and todorokite MnO₂ were confirmed by XRD (Fig. 7A), and the benzene oxidation reactions performed over the pristine and acid-treated samples are comparatively shown in Fig. 7(B–E). Except α-MnO₂, acid treatment significantly promoted benzene oxidation over the other three MnO₂ samples, especially for the todorokite MnO₂, but the acid-treated β-, α- (also the untreated one), todorokite and Aladdin MnO₂ were still less active than the acid-treated birnessite MnO₂ (H-MnO₂ (30-0.2-6)). The different effects of acid treatment and different extents, to which acid treatment could improve the benzene oxidation performance, might be largely dependent on the intrinsic properties of the studied samples. Future studies will be carried out to elucidate this issue.

4. Conclusions

In this study, catalytic oxidation of gaseous benzene over birnessite MnO₂ was investigated, and the great enhancement by HNO₃ treatment on benzene oxidation was clarified by various characterizations and specially designed experiments. The following conclusions could be drawn:

- (1) The sample which was treated by 0.2 M of HNO₃ aqueous solution at 30 °C for 6 h possessed the best catalytic performance with excellent water resistance, exhibiting a stable removal efficiency of 794% for 318 ppm of benzene under a high space velocity of 120 L·g⁻¹·h⁻¹ and 1.5 vol.% H₂O at 250 °C.
- (2) The acid treatment method for fabricating high-performance benzene oxidation catalyst is a convenient and green process because the pristine MnO₂ was prepared at low temperature and atmospheric pressure, and the acid treatment was carried out at ambient temperature with the HNO₃ solution being recycled over times without lowering the catalytic activity.
- (3) The increased acid sites and acidity of the acid-treated surface

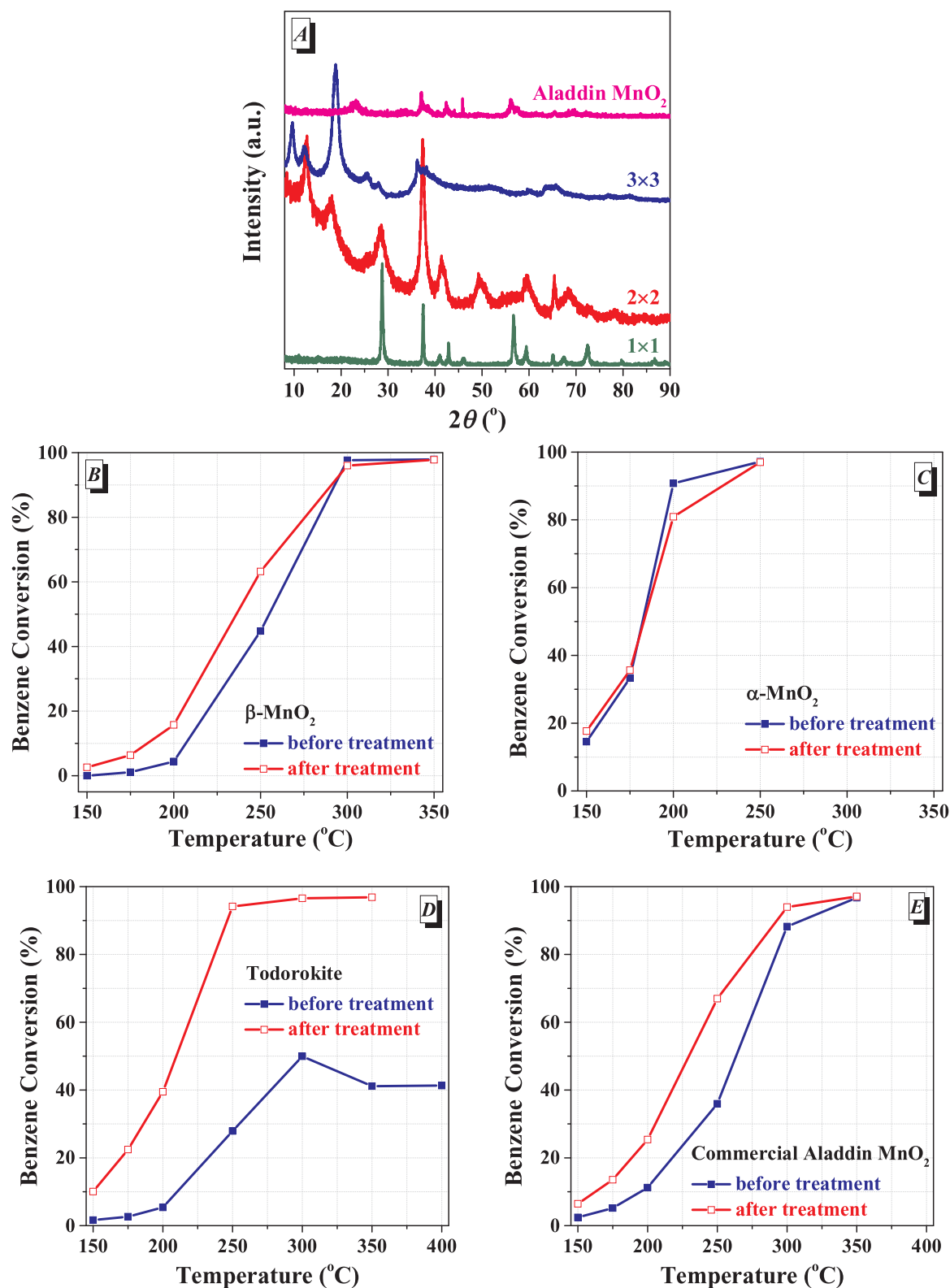


Fig. 7. Effects of acid treatment on benzene oxidation were investigated over $\beta\text{-MnO}_2$, $\alpha\text{-MnO}_2$, todorokite MnO_2 and commercial Aladdin MnO_2 to test the universality of the HNO_3 treatment method for benzene oxidation: (A) XRD patterns of the as-synthesized materials before acid treatment; (B) to (E) Benzene conversion vs. Reaction temperature. Benzene oxidation conditions were the same as those in Fig. 1A.

(pyridine adsorption IR) promoted the adsorption and activation of gaseous benzene ($\text{C}_6\text{H}_6\text{-TPD}$), and the lattice oxygen and surface adsorbed oxygen became more facile and reactive (surface oxidation reaction of benzene) due to the generated active oxygen vacancies via acid treatment (XPS, $\text{H}_2\text{-TPR}$ and $\text{O}_2\text{-TPD}$), these two

favorable factors together with the easy desorption of reaction products ($\text{CO}_2\text{-TPD}$) resulting in the excellent performance of the acid-treated sample.

(4) The acid treatment method adopted in this study was universal to other crystal structures of MnO_2 except $\alpha\text{-MnO}_2$, thereby paving

road for the preparation of active benzene decomposition catalysts with potential for practical application in the future.

Conflict of interest

There are no conflicts to declare.

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All the authors of this article would like to deliver their best wishes to the coming 70th founding anniversary of *Dalian University of Technology* since the year of 1949.

Appendix A. Supplementary data

Supplementary material related to this article can be found, in the online version, at doi:<https://doi.org/10.1016/j.apcatb.2019.01.023>.

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